# Implementation of a Speed Controlled Brushless DC Drive Using TMS320F240

Literature Number: BPRA064 Texas Instruments Europe July 1997

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# Implementation of a Speed Controlled Brushless DC Drive Using TMS320F240

#### ABSTRACT

The DSP Controller TMS320F240 from Texas Instruments is suitable for a wide range of motor drives. TMS320F240 provides a single chip solution by integrating on-chip not only a high computational power but, also, all the peripherals necessary for electric motor control. The main benefits are increased system reliability and cost reduction of the overall system. The present application note describes how a speed controlled brushless DC drive can be implemented using TMS320F240 and what kind of results can be achieved.

## 1. Introduction

Permanent magnet synchronous machines with trapezoidal Back-EMF and (120 electrical degrees wide) rectangular stator currents are widely used as they offer the following advantages: first, assuming the motor has pure trapezoidal Back EMF and that the stator phases commutation process is accurate, the mechanical torque developed by the motor is constant; secondly, the Brushless DC drives show a very high mechanical power density. This application report covers the TMS320F240 DSP Controller and some system considerations to get out high performances from a BLDC motor drive.

## 2. Brushless DC Drive Presentation

### 2.1. The Motor

The synchronous machine with permanent magnets used in this application note is a three phase Y wound motor. It has one magnetic pole pair on the rotor. The stator phase inductance is 40mH and the phase resistance is 190m $\Omega$ . The maximum permissible current at 5000rpm is 4.3A and the torque constant is equal to 17.2mNm/A. Its electromagnetic force waveform is trapezoidal and it is supplied with direct current. The DC bus voltage is 12V.

#### 2.2. The Control Hardware

The control hardware can be either the TMS320F240 Evaluation Module or the MCK240 introduced by Texas Instruments. In this application, the second board can be plugged directly onto the power electronics board. The two boards contain a DSP controller TMS320F240 and its oscillator, a JTAG and an RS232 link and the necessary output connectors. See the figure below which depicts the EVM board.

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Figure 1: Top View of TMS320F240 EVM Board

## 2.3. The Power Electronics Hardware

The power board is designed to support a 12V DC voltage supply and a 300W power range. The converter topology support either sinusoidal currents (Three phases ON operation) or direct currents (Two phases ON operation). The latter control method is implemented in this application note. Figure 3 shows the converter which is used here. The power switches use the power MOSFET, type IRFP054. The selected pre-driver component is the IR2131 and the PWM output signals coming from TMS320F240 are directly connected to the pre-driver without any additional buffer. The pre-driver output signals go through a resistor and then directly to the power switches. The relative ground of the upper half bridge is implemented with bootstrap capacitors. This hardware configuration allows hard chopping as well as soft chopping operation. All the elements for protection of the power device securities are provided: Shutdown, Fault, Clearfault, Itrip, reverse battery diode, varistor peak current protection. The current sensing is ensured by a low cost shunt resistor, its voltage drop is directly interfaced with the TMS320F240 as shown in Figure 3. The break feature is accomplished with another MOSFET and a power resistor. Finally, the power board supports the voltage supply for position sensors such as Hall effect sensors and incremental encoders.



Figure 2: Power Electronics Topology

The bold arrows on the wires depict the Direct Current flowing into two motor phases during the pulsed signals Turn ON.

#### 2.4. The Control Algorithm

According to Reference [3] (See list at the end of this report), torque production is almost directly proportional to the phase current. This statement gives rise to the following BLDC motor speed control scheme:



Figure 3: Speed & Current Control Loop Implemented in this Application

In this control scheme, torque production follows the principle that current should flow in only two of the three phases at a time. Only one current at a time needs to be controlled so that only one current sensor is necessary. The positioning of the current sensor allows the use of a low cost sensor as a shunt.

## 3. Sensing and Regulation

#### 3.1. Current Sensing

As shown in Figure 3, a shunt resistor is used to sense the current. The shunt is inserted between the sources of the power bridge lower side and the power board ground. Its value is set such that it activates the integrated over-current protection when the maximum current permitted by the power board has been reached. The voltage drop across the shunt resistor is converted by the dual ADC module, once it has been amplified to address the whole conversion range. The end of the conversion generates an interrupt flag (INT6 of the DSP Controller core) and the Interrupt Sub Routine is executed. The ADC reading for 30A will be 3FFh and for 0A will be 0h.

The phase current is sensed every 50µs in order to implement a 20kHz current loop. Each current measurement leads to a new PWM duty cycle loaded at the beginning of a PWM cycle. Note that, during Turn OFF, the shunt resistor does not have this current to sense, regardless of whether the inverter is driven in hard chopping or in soft chopping mode. The figure below depicts the shunt current in soft chopping mode and shows that in the Turn OFF operation the decreasing current flows through the M2 free wheeling diode and through the maintained closed M4 (so there is no current observable in the shunt in this chopping mode during Turn OFF). This implies that it is necessary to start a current conversion in the middle of the PWM duty cycle. The TMS320F240 event manager can handle this by starting a conversion on the Timer1 (dedicated in this application to PWM unit) period match.



Figure 4: Shunt Resistor Voltage Drop according to PWM DutyCycles (Soft Chopping)

In the hard chopping mode during the Turn OFF neither M1 nor M4 drive current, so that the decreasing phase current flows from ground through the shunt resistor via M2 and M3 free wheeling diodes and back to ground via the capacitor. In this chopping mode it is possible to see the exponentially decreasing phase current across the shunt as a negative shunt voltage drop appears. Assuming that neither the power board nor the control board support negative voltages, this necessitates that the current be sensed in the middle of the Turn ON.

### 3.2. Position Sensing

The motor in this application is equipped with three Hall effect sensors. These sensors are fed by the power electronics board. The sensor outputs are directly wired to the TMS320F240 Capture Unit. This unit is configured by software to capture 4 inputs (only 3 necessary) and not like QEP. Timer2 is selected as the time base for the capture unit. As this is set in continuous up-count mode and as the slowest reachable speed is governed by the largest acceptable period, T2PER (Timer 2 Period) register is set to 0xFFFEh and the prescaler is set to 128. This setting allows the speed to go down to 24rpm (with CPUCLOCK=20MHz). The Hall effect sensors give three 180° overlapping signals, thus providing the six mandatory commutation points: The rising and falling edges of the sensor output are detected, the corresponding interrupt flag is generated and the Interrupt Sub Routine is served (Event Manager Interrupt group C). The ISR first

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determines which edge has been detected, then computes the time elapsed since the last detected edge and commutates the supplied phases.

#### 3.3. Speed Sensing

The speed feedback is derived from the position sensor output signals. As mentioned in the previous paragraph, there are six commutation signals per mechanical revolution. In other words, between two commutation signals there are 60° mechanical degrees. As the speed can be written as:

$$\Delta\theta / \Delta T$$

where  $\theta$  is the mechanical angle it is possible to get the speed from the computed elapsed time between two captures. Between two commutation signals the angle variation is constant as the Hall effect sensors are fixed relative to the motor, so speed sensing is reduced to a simple division. It is possible to overcome the floating point characteristic of the F240 DSP Controller with extended arithmetic algorithms to perform the division, but in this application a simple 16 bits division is sufficient. In addition, the error caused by neglecting the division remainder becomes smaller as the speed increases.

#### 3.4. Current Regulation

Current regulation is achieved by Pulse Width Modulation (fixed frequency 20kHz) signals with varying duty cycles. PWM width is determined by comparing the measured phase current with the desired reference current as shown below:

$$I_{error} = I_{ref} - I_{measured}$$
  

$$duty\_cycle_{new} = duty\_cycle_{old} + I_{error} \times K$$
  
if  $duty\_cycle_{new} \ge Timer\_period$   
then  

$$duty\_cycle_{new} = Timer\_period$$
  
if  $duty\_cycle_{new} \le O$   
then  

$$duty\_cycle_{new} = O$$

where, K is the proportional gain and depends on motor parameters and also on DC bus voltage and currents. The proportional gain K can be determined using the following procedure.

Let *S* be the number of steps allowed in one PWM cycle. Let  $\Delta i$  be the change in phase current for 100% change in PWM duty cycle. The proportional gain, *K*, can be defined as:

$$K = \frac{S}{\Delta i}$$

parameter  $\Delta i$  depends on motor and converter types.

#### 3.5. Speed Regulation

The speed regulation loop is executed once every 62.5ms. This frequency can be modified according to the need of the application. In this control software the speed reference is directly written into memory space. It is possible to get the speed reference from an external potentiometer or from PC interface by using a ADC channel or the RS232 serial link. The new direct current reference is computed from the speed error and by means of a common digital *PI* algorithm:

$$Idcref_{k} = Idcref_{k-1} + Kp(E_{k} - E_{k-1}) + KiTE_{k-1}$$

where *Idcref* is the speed regulator output, Kp the proportional gain, Ki the integral gain and T the speed sampling period. The sampling period is equal to 0.0625 that is to say  $2^{-4}$ . From a numerical standpoint the multiplication KiT is done by right shifting the integral term four times before adding it to the others. See below for management of other speed loop sampling frequencies.

In the speed loop code every variable is stored into a stack. The stack pointer used is the auxiliary register AR2 and the stack entry address is 0x0300h.

STACK ADDRESS	VARIABLE
0x0300h	Capture k instant
0x0301h	Capture k-1 instant
0x0302h	Time elapsed between Capture k and k-1
0x0303h	Speed error k
0x0304h	Speed error k-1

#### Table 1: Speed Loop Variables Stack

## 4. Startup Operation

At zero speed the control software has first to determine which phase it should supply. So first of all the code reads the three Hall effect sensor output sequence and applies a voltage on the appropriate phase pair. This operation causes the motor to start rotating. The supplied phase pair is then changed at each Hall sensor output edge. The applied current does not change until the first speed loop entry. The user may want to immediately update the current reference, in this case just set *speed\_count* to the speed loop frequency in the variable initialization.

## 5. **PWM Strategy and Generation**

The motor in this application is fed with Direct Current and two phases ON. In other words one phase feeds the motor with current, another phase is the current return path and the third phase is opened (See Figure 2). So at any time there are only two power switches conducting current. Let M1 and M4 be the switch pair considered. There are two ways to get the desired current into the right phase pair: either hard chopping or soft chopping operation. In the case of soft chopping the M4 power switch is maintained closed during all the 60° commutation while M1 switches according to the current loop output duty cycle. In the hard chopping case both M1 and M4 switch according to the same pulsed pattern. TMS320F240 supports the two chopping operation as proven below.

Soft chopping mode with CPUCLOCK=20MHz, PWM period=20kHz, PWM duty cycle = comp, active switches M1 and M4.

LACC	COMP
LDP	#0E8h
SPLK	#0F3Dh,ACTR
SACL	CMPR1
SPLK	#0000, CMPR2
SPLK	#0000,CMPR3

Hard chopping mode with CPUCLOCK=20MHz, PWM period=20kHz, PWM duty cycle = comp, active switches M1 and M4.

LACC	COMP
LDP	#0E8h
SPLK	#0F7Dh,ACTR
SACL	CMPR1
SACL	CMPR2
SPLK	#0000,CMPR3

Discussion of the advantages of one chopping mode versus another is beyond the scope of this application note. Hard chopping has been implemented here.

## 6. Experimental Results

The three following pictures show the current regulation results. The current reference was set to 1A, 2A and 4A respectively. The scope channel #4 is the phase A current measured by a current probe. The scope channel #3 is the phase A terminal voltage (this voltage has been measured between the phase A half bridge and the power board ground). This voltage is sensed directly on the upper side switch source. These figures show very small dV/dt and dI/dt.



Figure 5: Current Regulation Results

The next two Figures are the Phase A current and half bridge voltage measured as the motor runs with closed loop speed control and a speed reference set to 700rpm. Two alternative braking torques are available to the regulation loop: 0.03 and 0.06Nm (Maximum Produced Torque =Torque constant \* maximum continuous current =  $17.2^{*}4.37 = 75.2$ mNm).



Figure 6: Speed Regulation Results (Spdref = 700rpm)

The next two pictures shows the motor running closed loop at the reference speed of 1500rpm with different braking torque (0.03, 0.06Nm respectively 40% and 80% of the maximum torque).



Figure 7: Speed Regulation Results (Spdref=1500rpm)

The last following figure shows the motor running closed loop at the reference speed of 2300rpm and its maximum deliverable torque.



Figure 8: Speed Regulation Results (Spdref=2300rpm)

The speed response time in this application is below 2 seconds and the speed ripple is below 2%. The tested speed range is from 100rpm to 3000rpm.

## 7. How to Use the Code in another Application

The code given in the next chapter is suitable for one BLDC motor drive with constant braking torque and very high load inertia. As system parameters such as motor phase resistance and electrical and mechanical time constants change with the application, the software may be improved to get the best performances. The main part to change will probably be the regulator coefficients and the output limitation.

## 7.1. Current Regulator

As seen in chapter 3.4 the current regulator output is

```
duty\_cycle_{new} = duty\_cycle_{old} + I_{error} \times K
```

In the present software the gain K is set to 1. It may be very easily set to  $2^x$  by right or left shifting the current error. If another factor is needed a new coefficient K should be set at the start of the software and the code should be modified as below

```
;Current error calculation
      CLRC
              SXM
      LACC
              ADCFIF01,10
      LDP
              #0
      SUB
              Idc ref,16
      SETC
              SXM
;Current regulator
      SACH
              Idc
      ЪТ
              Idc
      MPY
              #Κ
      PAC
              COMP
      ADD
      SACL
              COMP
```

### 7.2. Speed Regulator

As the speed regulator implemented is a common *PI* algorithm, there are three parameters free to be changed in order to get good dynamic behaviour: the speed loop frequency *T*, the proportional gain  $K_p$  and the integral gain  $K_i$ . As a first step, only  $K_p$  and  $K_i$  should be adapted. Then it may be necessary to increase the speed loop frequency: change the maximum value of *speed\_count* variable and pay attention to the *KiT* numerical dynamic.

The user may want a speed error limitation in order to avoid either numerical overflows or a too high input current. The following code performs this limitation and is inserted between the end of Speed and speed error calculation block and Speed regulator:

```
LAR AR2,#0303h
BGEZ LIMIT
ABS
SPLK #-1,SPEED_COUNT
LIMIT
```

```
SACL *
SUB #01Ah ;0X01Ah is the max speed error
BLEZ OK
SPLK #01Ah,*
OK
LT SPEED_COUNT
MPY *
PAC
```

A very similar code can be used to limit either the speed regulator output or the output rate of change.

## 8. BLDC Motor Drive Code

#### 8.1. Assembly Code

There are seven variables used in this software. The CAPT variable is used by the SEQUENCE sub routine to determine which 60° sector the rotor is in and thus activate the correct pulsed signal pair. The COMP variable is the duty cycle update, it varies from 0 to 500 in this application. Notice that the closer to zero this value becomes, the bigger the phase current. Idc is the variable used to store the line current sensed by means of the ADC module and of the voltage drop across the shunt resistor. Idc\_ref is the speed regulator output. It can be interpreted as the torque reference value given by the speed regulation. SPEED REF is the variable in which the reference speed value can be stored. This reference may come from the conversion of an external potentiometer voltage drop or from an user interface (the speed reference can be set via serial communication from a PC for example). SPEED COUNT is a software counter (software clock frequency is equal to the PWM frequency 20kHz) which determines the speed regulation loop period. This variable can be set into the Current end of conversion Interrupt subroutine. Changing the counter period value also means changing the speed regulator integral gain. The final stack variable is the start address of the context switching necessary software stack. The memory space allocated to this stack is 6, so that it can be stored up to 6 registers.

;Speed regulator coefficients setting ;-----Кp .set 015 .set Κi 004 ; Variable definitions ; Capture indication
;Duty cycle .bss CAPT,1 .bss COMP,1 .bssIdc,1;Line current.bssIdc\_ref,1;Current reference.bssSPEED\_REF,1;Speed reference SPEED\_COUNT,1 ; Speed loop frequency .bss stack,6 ;Context save stack .bss ; Reset & interrupt vectors .sect "vectors" \_c\_int0 ; PM 0 Reset Vector RSVECT В .space 16\*6 INT4 В CAPINT .space 16\*2 INT6 В ADCINT .space 16\*38 .text .global \_c\_int0 \_c\_int0 SETC CNF CLRC OVM ; Reset overflow mode SETC SXM ; Reset sign extension mode CLRC XF SETC INTM ; Set global interrupt mask MAR \*,AR2 ;Init speed variables stack LAR AR2,#0300h SPLK #0,\*+ #0,\*+ SPLK SPLK #OFFFFH,\*+ SPLK #029H,\*+ SPLK #029H,\*+ SPLK #0,\* AR2,#0300h LAR LAR AR1,#stack ;Init context save stack pointer ;Disable watchdog (Vccp=5v)& watchdog counter reset p6-12 LDP #00E0h SPLK #0006Fh, WD\_CNTL SPLK #05555h, WD KEY #0AAAAh, WD KEY SPLK ; initialize WDT registers

#06Fh, WD\_CNTL ; clear WDFLAG, Disable WDT, set WDT SPLK ; for 1 second overflow. ; Set up CLKOUT to be SYSCLK p6-6 SPLK #40C0h,SYSCR LACC SYSSR AND #069FFh SACL SYSSR ;set up PLL clockin=10Mhz,CPUCLOCK=20Mhz,SYSCLK=10Mhz SPLK #0002h,CKCR0 ; PLL disabled SPLK #00b1h,CKCR1 SPLK #0081h,CKCR0 ;Set up zero Wait States for external memory MAR \*,AR1 #0008h LACC SACL \* OUT \*,WSGR ;I/O setting pl1-11 #00E1h LDP #0000fh, OCRA SPLK SPLK #0070h, OCRB SPLK #02800h, PBDATDIR ; not shut down clearing fault LACC PBDATDIR ; Clear EV control registers LDP #0E8h #0000h,T1CON ;no timer enable SPLK SPLK #0000h,T1PER SPLK #0000h,T1CNT SPLK #0000h,T1CMP SPLK #0000h,T2CON SPLK #0000h,T2PER SPLK #0000h,T2CNT #0000h,T2CMP SPLK SPLK #0000h,T3CON SPLK #0000h,T3PER SPLK #0000h,T3CNT #0000h,T3CMP SPLK SPLK #0000h,COMCON SPLK #0000h,DBTCON SPLK #0000h,ACTR SPLK #0000h,SACTR #0000h,CMPR1 SPLK #0000h,CMPR2 SPLK #0000h,CMPR3 SPLK SPLK #0000h,SCMPR1 SPLK #0000h,SCMPR2 #0000h,SCMPR3 SPLK SPLK #0000h,CAPCON ;no capture #00ffh,CAPFIFO SPLK LACC FIFO1 LACC FIFO2

;

;

;

;

LACC FIFO3 ;GP Timer 2 Setting start with GPT1 presc 128 #0fffeh,T2PER SPLK SPLK #00000h,T2CNT SPLK #17C0h,T2CON ;PWM Unit setting #00500,T1PER SPLK SPLK #0000h,T1CNT #0FFFh,ACTR SPLK SPLK #0508h,DBTCON #00000,CMPR1 SPLK SPLK #00000,CMPR2 SPLK #00000,CMPR3 #0287h,COMCON SPLK SPLK #8287h, COMCON SPLK #2800h,T1CON SPLK #2840h,T1CON SPLK #0100h,GPTCON ;Capture Unit Setting SPLK #0b0fch,CAPCON SPLK #00ffh,CAPFIFO ;Core Mask Setting LDP #0 LACC #028h IMR SACL LACC IFR SACL IFR ;EV Mask Setting, Vector & Flag reset p11-46 LDP #0E8h LACC IFRA SACL IFRA LACC IFRB SACL IFRB LACC IFRC SACL IFRC SPLK #0,IMRA SPLK #0,IMRB SPLK #7, IMRCLACC IVRA LACC IVRB IVRC LACC ;ADC Unit setting p3-8 LDP #0E0h #0403h, ADCTRL2 SPLK SPLK #1b0ah,ADCTRL1 ;ADCIN5 CLRC INTM

LDP #0 ;Variables init SPLK #001FH,Idc\_ref SPLK #040H,SPEED REF SPLK #0500,COMP SPLK #0000, SPEED\_COUNT #0000H,CAPT SPLK \*STARTING PROCEDURE\* ;Disable CAPT Input p2-75 LDP #0E8h SPLK #8000h,CAPCON SPLK #00ffh,CAPFIFO ;Set I/O unit as I LDP #00E1h #0FF00h, OCRB SPLK #0000h, PCDATDIR SPLK ;WHICH SEQUENCE? LACC PCDATDIR AND #0070H LDP #0 SACL CAPT LACC CAPT,12 CAPT SACH ;Disable I/O Unit LDP #0E1h SPLK #0FF70h, OCRB ;Capture Unit Setting LDP #0E8H #0b0fch,CAPCON SPLK SPLK #00ffh,CAPFIFO

* * * * * * * * * * * * * * * *	* * * * * * * * *	* * * * * * * * * * * * * * * * * *	* * *
*END OF STARTIN		JRE* * * * * * * * * * * * * * * * * * * *	* * *
FAULT_CLEAR	LDP LACC AND BZ SPLK LDP	#0E1h PBDATDIR #010h FAULT_CLEAR #02820h,PBDATD: #0E8h	;Init the pre-driver IR
LOOP	NOP NOP B	LOOP	;Polling loop
SEQUENCE			
	LDP LACC SUB SFL ADD BACC	#0 CAPT #1 #CAPT_DETER	
CAPT_DETER			
	B B B B B	FALLING3 FALLING1 RISING2 FALLING2 RISING1	
RISING3			
	LACC LDP SPLK SACL SACL SPLK B	COMP #0E8h #0DF7h,ACTR CMPR3 CMPR1 #0000,CMPR2 END	
FALLING3		601F	
	LACC LDP SPLK SACL SACL SPLK B	COMP #0E8h #07FDh,ACTR CMPR1 CMPR3 #0000,CMPR2 END	
RISING2			
	LACC LDP SPLK SACL SACL	COMP #0E8h #07DFh,ACTR CMPR2 CMPR3	

			#0000,CMPR1
		В	END
FALLING2		LACC	COMP
		LDP	
			#0D7Fh,ACTR
		SACL	CMPR3
			CMPR2
			#00000,CMPR1
		B	END
RISING1		2	
		LACC	COMP
		LDP	#0E8h
		SPLK	#0F7Dh,ACTR
		SACL	CMPR1
		SACL	CMPR2
		SPLK	#0000,CMPR3
		В	END
FALLING1			
		LACC	COMP
		LDP	#0E8h
		SPLK	#0FD7h,ACTR
		SACL	CMPR2
		SACL	
		SPLK	#00000,CMPR3
END			
		RET	
SPEED_REG		MAD	* 302
		MAR	
		LAR	
		LDP	#0 #1 CDEED COINE
		SPLK	#1,SPEED_COUNT
	;Speed	and spee	ed error calculation
	-		SXM
		ZAC	
		OR	#0FFFFH
		RPT	#15
		SUBC	*
		AND	#OFFFFH
		SUB	SPEED_REF
		NEG	
		SETC	SXM
	;Speed	regulati	
		LAR	AR2,#0303h
		SACL	*+
		SUB	*+ *
		SACL	*_
		LT MDV	
		MPY T TTD	#Кр *_
		LTP MPY	^_ #Кі
		1.1T T	ПТСТ

LTD \* ADD Idc\_ref,4 SFR SFR SFR SFR SACL Idc\_ref ;Reset Speed loop timer SPLK #0,SPEED\_COUNT ;Restore AR2,#0300H LAR RET ADCINT ;save status registers \*,AR1 MAR \*+ ; skip one position MAR #1, \*+ SST ; save ST1 SST #0, \* ; save STO LDP #0 LACC SPEED\_COUNT SUB #1250 BNZ NO\_SPEED\_REG CALL SPEED\_REG NO\_SPEED\_REG LACC SPEED\_COUNT ADD #1 SACL SPEED\_COUNT LDP #0E0h LACC SYSIVR ;current error calculation CLRC SXM LACC ADCFIF01,10 LDP #0 SUB Idc\_ref,16 SETC SXM ;current proportional regulator ADD COMP,16 SACH COMP ; current regulator output limitation LACC COMP BGZ SUP\_LIM SPLK #0,COMP В COMP\_OK SUP\_LIM SUB #0500 COMP\_OK BLZ

SPLK #0500,COMP COMP\_OK ;output PWM CALL SEQUENCE ;restore status registers MAR \*, AR1 ; make stack pointer active LST #0, \*- ; load ST0 LST #1, \*- ; load ST1 CLRC INTM RET CAPINT MAR \*,AR1 \*+ ; skip one position MAR ; save ST1 ; save ST0 SST #1, \*+ #0, \* SST ;Capture interrupt handling LDP #0E8h LACC IVRC ;FLAG RESET ; speed calculation MAR \*, AR2 LACL T2CNT SACL \*+ SUB \*+ \* \_ SACL \* ADD \* \_ SACL ;Disable CAPT Input p2-75 LDP #0E8h SPLK #8000h,CAPCON SPLK #00ffh,CAPFIFO ;Set I/O unit as I #00E1h LDP SPLK #0FF00h, OCRB SPLK #0000h, PCDATDIR ;WHICH SEQUENCE? LACC PCDATDIR #0070H AND LDP #0 SACL CAPT LACC CAPT, 12 SACH CAPT ;Commutation

CALL SEQUENCE

```
;Disable I/O Unit
     LDP #0E1h
      SPLK
            #0FF70h, OCRB
;Capture Unit Setting
      LDP
            #0E8H
      SPLK
             #0b0fch,CAPCON
      SPLK
             #00ffh,CAPFIFO
      MAR
             *, AR1
                           ; make stack pointer active
                           ; load STO
      LST
            #0, *-
             #1, *-
                           ; load ST1
      LST
      CLRC
             INTM
      RET
```

#### 8.2. Linker File

MEMORY { : origin = 0h , length = 040h /\* PROGRAM \*/ PAGE 0 : VECS PROG : origin = 40h , length = 0800h /\* Ext mem \*/ PAGE 1 : MMRS : origin = 0h , length = 05Fh /\* MMRS \*/ / \* DARAM / \* DARAM / \* DARAM / \* DARAM в2 : origin = 0060h , length = 020h\* / : origin = 0100h , length = 0200h в0 \* / : origin = 0300h , length = 0200hВ1 \*/ }

```
/*-----*/
/* SECTIONS ALLOCATION */
/*-----*/
SECTIONS
{
    .vectors : { } > VECS PAGE 0 /* INTERRUPT VECTOR TABLE */
    .text : { } > PROG PAGE 0 /* CODE */
    .mmrs : { } > MMRS PAGE 1 /* Memory Mapped Registers */
    .blk0 : { } > B0 PAGE 1 /* Block B0 - page 4 */
    .bss : { } > B2 PAGE 1 /* Block B2 - page 0 */
    .blk1 : { } > B1 PAGE 1 /* Block B1 - page ? */
}
```

#### 8.3. Header File

; File Name: C240APP.H ; Project: C240 EVM Apps S/W suite ; Originator/s: Auto/Ind DSP Apps group - Texas Instruments (Houston) ; ; Description: C240 Header file with all Peripheral Register declarations ;------; On Chip Peripheral Register Definitions (DATA SPACE) ;C2xx Core Registers .set 0004h .set 0005h .set 0006h 0004h 0005h ;Int Mask Register ;Global memory allocation reg IMR GREG IFR ;Int Flag Register

# ;System Module Registers

SYSCR	.set	07018h	;System Module Control Register
SYSSR	.set	0701Ah	;System Module Status Register
DIN	.set	0701Ch	;Device Identification Register
SYSIVR	.set	0701Eh	;System Interrupt Vector Register
XINT1_CNTL	.set	07070h	;Intl (type A) Control reg
NMI_CNTL	.set	07072h	;Non maskable Int (type A)
XINT2_CNTL	.set	07074h	;Int2 (type C) Control reg
XINT3_CNTL	.set	07076h	;Int3 (type C) Control reg
PDPINT_CNTL	.set	0742Ch	; Power Drive Protection Int cntl reg

#### ;Digital I/O

;~~~~~~~~			
OCRA	.set	07090h	;Output Control Reg A
OCRB	.set	07092h	;Output Control Reg B
PADATDIR	.set	07098h	;I/O port A Data & Direction reg.
PBDATDIR	.set	0709Ah	;I/O port B Data & Direction reg.
PCDATDIR	.set	0709Ch	;I/O port C Data & Direction reg.
PDDATDIR	.set	0709Eh	;I/O port D Data & Direction reg.

WSGR	.set	OFFFFh	;Wait State Generator Register
------	------	--------	--------------------------------

;Watch-Dog(WD) / Real Time Int(RTI) / Phase Lock Loop(PLL) Registers

;~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~				
RTI_CNTR	.set	07021h	;RTI Counter reg	
WD_CNTR	.set	07023h	;WD Counter reg	
WD_KEY	.set	07025h	;WD Key reg	
RTI_CNTL	.set	07027h	;RTI Control reg	
WD_CNTL	.set	07029h	;WD Control reg	
CKCR0	.set	0702Bh	;PLL control reg 0	
CKCR1	.set	0702Dh	;PLL control reg 1	

;Analog-to-Digital Converter(ADC) registers

;~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~				
ADCTRL1	.set	07032h		
ADCTRL2	.set	07034h		
ADCFIF01	.set	07036h		
ADCFIFO2	.set	07038h		

;Event Manager (EV) - EV Base Address = 0x7400

	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~		~~~~~~
EV_BASE	.set	7400h	; Event Manager Base Address
GPTCON	.set	00h + EV_BASE	; General Timer Controls
T1CNT	.set	01h + EV_BASE	; T1 Counter Register
T1CMP	.set	02h + EV_BASE	; T1 Compare Register
T1PER	.set	03h + EV_BASE	; T1 Period Register
T1CON	.set	04h + EV_BASE	; T1 Control Register
T2CNT	.set	05h + EV_BASE	; T2 Counter Register
T2CMP	.set	06h + EV_BASE	; T2 Compare Register
T2PER	.set	07h + EV_BASE	; T2 Period Register
T2CON	.set	08h + EV_BASE	; T2 Control Register
T3CNT	.set	09h + EV_BASE	; T3 Counter Register
T3CMP	.set	0ah + EV_BASE	; T3 Compare Register
T3PER	.set	0bh + EV_BASE	; T3 Period Register
T3CON	.set	0ch + EV_BASE	; T3 Control Register
COMCON	.set	11h + EV_BASE	; Compare Unit Control
ACTR	.set	13h + EV_BASE	; Compare Unit Output Action Control
SACTR	.set	14h + EV_BASE	; S Comp Unit Output Action Control
DBTCON	.set	15h + EV_BASE	; Dead Band Timer Control
CMPR1	.set	17h + EV_BASE	; Compare Channel 1 Threshold
CMPR2	.set	18h + EV_BASE	; Compare Channel 2 Threshold
CMPR3	.set	19h + EV_BASE	; Compare Channel 3 Threshold
SCMPR1	.set	lah + EV_BASE	; S Comp Channel 1 Threshold
SCMPR2	.set	1bh + EV_BASE	; S Comp Channel 2 Threshold
SCMPR3	.set	lch + EV_BASE	; S Comp Channel 3 Threshold
CAPCON	.set	20h + EV_BASE	; Capture Unit Control
CAPFIFO	.set	22h + EV_BASE	; FIFO1-4 Status Register
FIFO1	.set	23h + EV_BASE	; Capture Channel 1 FIFO Top
FIFO2	.set	24h + EV_BASE	; Capture Channel 2 FIFO Top
FIFO3	.set	25h + EV_BASE	; Capture Channel 3 FIFO Top
FIFO4	.set	26h + EV_BASE	; Capture Channel 4 FIFO Top
IMRA	.set	2ch + EV_BASE	; Group A Interrupt Mask Register
IMRB	.set	2dh + EV_BASE	; Group B Interrupt Mask Register
IMRC	.set	2eh + EV_BASE	; Group C Interrupt Mask Register
IFRA	.set	2fh + EV_BASE	; Group A Interrupt Flag Register

IFRB	.set	30h + EV_BASE ; Group B Interrupt Flag Register
IFRC	.set	31h + EV_BASE ; Group C Interrupt Flag Register
IVRA	.set	32h + EV_BASE ; Group A Int. Vector Offset
IVRB	.set	33h + EV_BASE ; Group B Int. Vector Offset
IVRC	.set	34h + EV_BASE ; Group C Int. Vector Offset

## 9. Summary

This application report deals with a BLDC motor drive based on the DSP Controller TMS320F240 manufactured by Texas Instruments. The electronic commutation is accomplished by three Hall effect sensors directly wired to the DSP Controller capture Unit. Accurate current regulation is maintained with help of the ADC unit and the speed regulation is performed by the DSP core. This software solution might be considered as a starting point to design a permanent magnet synchronous machine drive with trapezoidal Back-EMF and rectangular stator currents.

## References

- 1. TMS320C24x DSP Controllers Reference Set: Vol.1, Texas Instruments Inc., 1997.
- 2. TMS320C24x DSP Controllers Reference Set: Vol.2 Texas Instruments Inc., 1997.
- 3. Digital Signal Processor Solutions for BLDC motor, Application Report Texas Instruments part #BPRA055.
- 4. Brushless Permanent Magnet Motor Design Duane C. Hanselman, McGraw Hill, Inc.