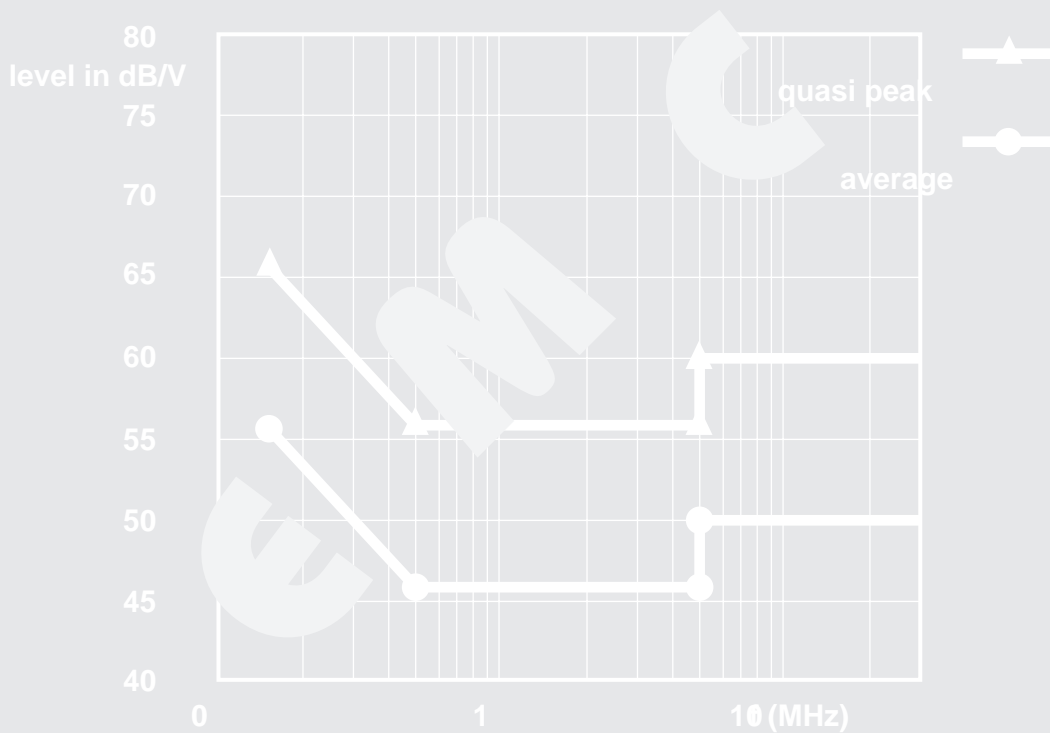


The Use of Soft Ferrite for Interference Suppression

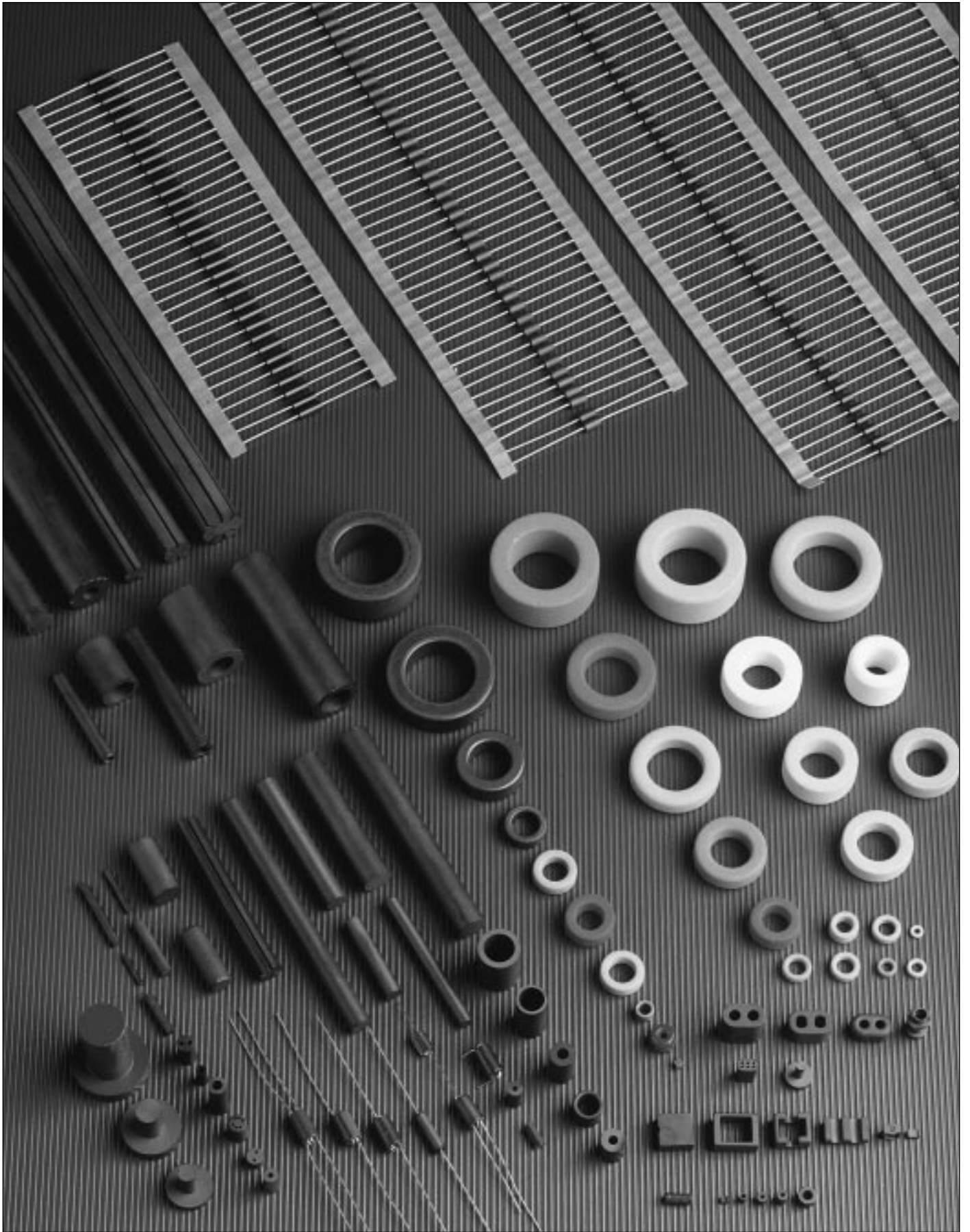


Let's make things better.

The Use of Soft Ferrites for Interference Suppression

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Assortment of EMI-suppression ferrite products

1. Introduction

In the field of electromagnetic compatibility several trends attribute to a growing necessity of EMC engineering.

In signal processing :

- Change from analog to digital (steep pulse edges, overshoot, ringing).
- Increase of clock frequencies.

In power conversion :

- Change from linear to switched-mode supplies (high switching frequency, harmonics).
- Increase of switching frequencies.

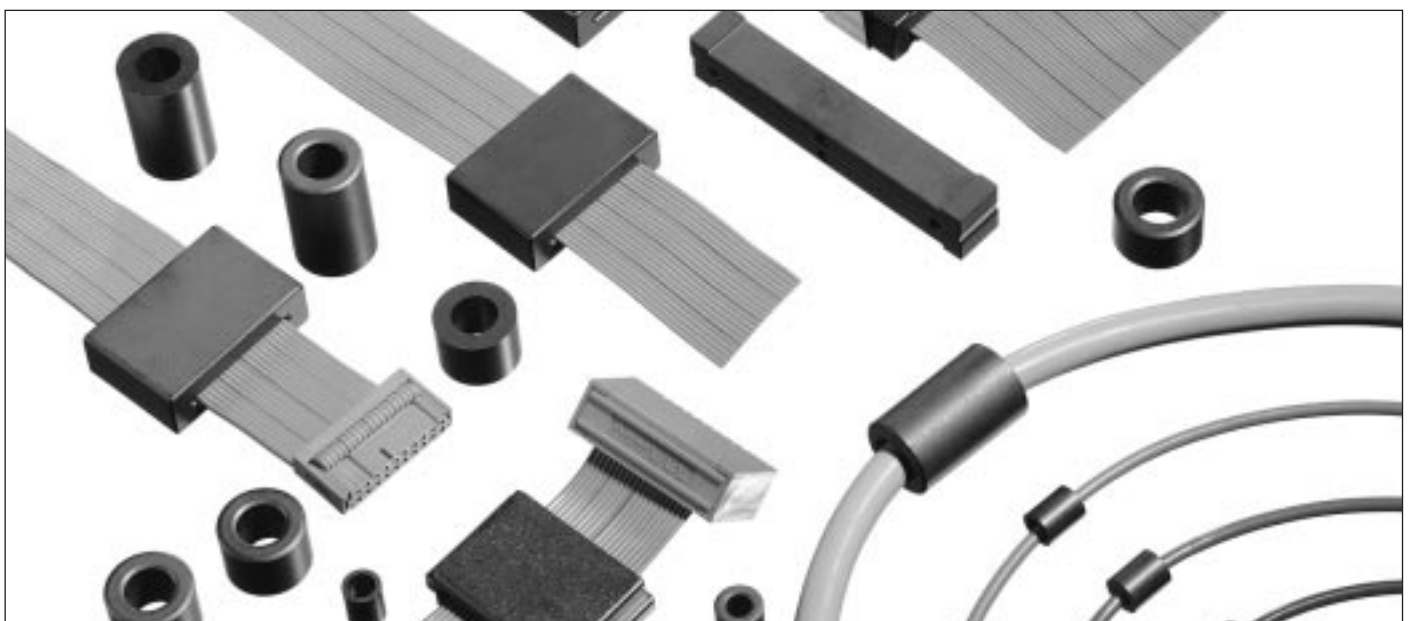
These trends, directed to functional upgrading or reducing cost, inevitably also contribute to an increasing level of electromagnetic interference (EMI) emissions. Together with the increasing use of electronics this leads to a general EMC degradation. As a consequence, EMC legislation is getting more strict in many countries.

The most important regulations are VDE in Germany, FCC in United States and VCCI in Japan. There is a uniform legislation in the European Community along the lines of the EMC directive 89/336/EEC. For every product to which no specific European norm applies, a general regulation is mandatory. These are the so called Generic Requirements (residential, commercial and light industry: EN 50081-1 for emissions and EN 50082-1 for immunity). This includes all electric and electronic products, no matter how trivial they seem to be !

Of course the first step to avoid interference problems is a good design practice, to tackle the problem right from the start. This can be insufficient if the interference is directly related to the inherent operating principle and too late if the interference is detected not earlier than in the final design phase. In such cases extra suppression components are necessary, like ferrites, capacitors or shielding elements. Ferrites provide a solution to many problems of conducted interference. They can be applied almost anywhere :

- Shifted on wire or cable as beads, tubes or cable shields.
- Mounted on PCB as beads-on-wire, wideband chokes or SMD inductors.
- Ring cores or U cores in mains filters, in the circuit, in a separate box or moulded in a connector.
- Wideband chokes or coiled rod inductors in electrical appliances or motors.

No earth connections are necessary as ferrites are connected in series with the interfering circuit and not in parallel as in the case of a capacitor. The wideband, lossy impedance makes ferrites well-suited as RF suppressor component.



2. General principles of EMC

2.a. Regulations

Historically, all EMI regulations stated emission limits only. These define the maximum level of interference allowed as a function of frequency.

In case of conducted interference it applies to the voltage on all inputs and outputs of the equipment, in case of radiated interference it applies to the field strength at a certain distance. Often two levels are stated :

- Class A for commercial and industrial areas.
- Class B for domestic and residential areas.

Class B is always stricter than class A. Recently, also immunity is becoming subject of regulation. Taking into account the severity of the EMC problem, equipment must also be able to operate without functional degradation in a minimum EMI ambient. The difference between the actual level of emissions or susceptibility and the EMC limits is the required attenuation by filtering or shielding.

2.b. Sources and propagation

The source determines whether the interference is a transient or random variation in time (commutation motors, broadcast transmitters etc.) or a periodic signal (e.g. switched-mode power supplies). The frequency spectrum will be continuous in the first case and a line spectrum in the second. In practice, the minimum and maximum frequency involved are much more relevant and both types of sources can be broadband. Random variations are broadband if they are very fast, harmonic disturbances if the basic frequency is high or if the deviation from a sine wave is considerable.

Interferences can propagate as an electromagnetic wave in free space. Suppression then requires shielding with conductive materials. Also propagation occurs via conductive paths such as the mains network, to which the majority of electrical equipment is connected. Below 30 MHz this is the main propagation mode. Suppression is done with a high impedance in series (inductor), a low impedance in parallel (capacitor) or a combination of both (filter).

Propagation via the mains can take place in two different modes: common and differential mode. Apart from phase and null which carry the supply current, there is the safety earth connection, which is generally taken as a reference.

Common-mode :

Phase and null interference voltages are equal. This is likely to occur if phase and null are close together and interference is coupling in from an external field (radiation or crosstalk).

Differential-mode :

Phase and null interference voltages have opposite phase angle but equal magnitude. This is likely to occur in case of switching equipment connected to the mains. In general a combination of both types can be present.

2.c. Suppression with ferrites

At RF frequencies a ferrite inductor shows a high impedance which suppresses unwanted interference. The resulting voltage over the load impedance will be lower than without suppression component, the ratio of the two is the insertion loss, see Fig.2.

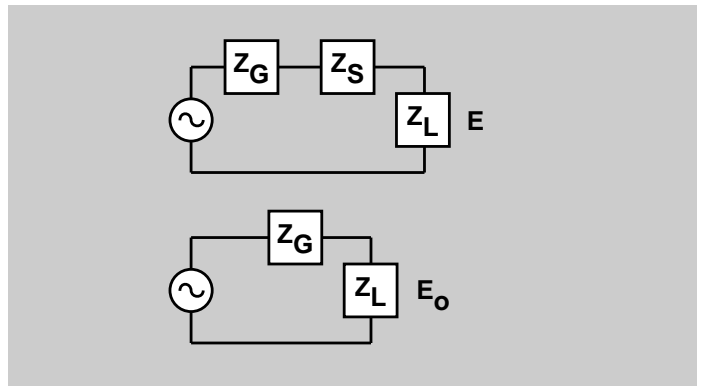


Fig. 2 Insertion loss of an inductor.

The insertion loss is expressed as:

$$\begin{aligned} \text{IL} &= 20 \cdot \log_{10} (E_0/E) \quad [\text{dB}] \\ &= 20 \cdot \log_{10} \frac{|Z_G+Z_L+Z_S|}{|Z_G+Z_L|} \quad [\text{dB}] \end{aligned}$$

where \$E\$ is the voltage on the load with inductor and \$E_0\$ without.

The decibel (dB) as a unit is practical because interference levels are also expressed in dB. However insertion loss depends on source and load impedance, so it is not a pure product parameter like impedance (\$Z\$). In the application, source and load impedance generally are not 50 \$\Omega\$ resistive. They might be reactive, frequency dependent and quite different from 50 \$\Omega\$.

Conclusion : insertion loss is a standardized parameter for comparison, but it will not predict directly the attenuation in the application.

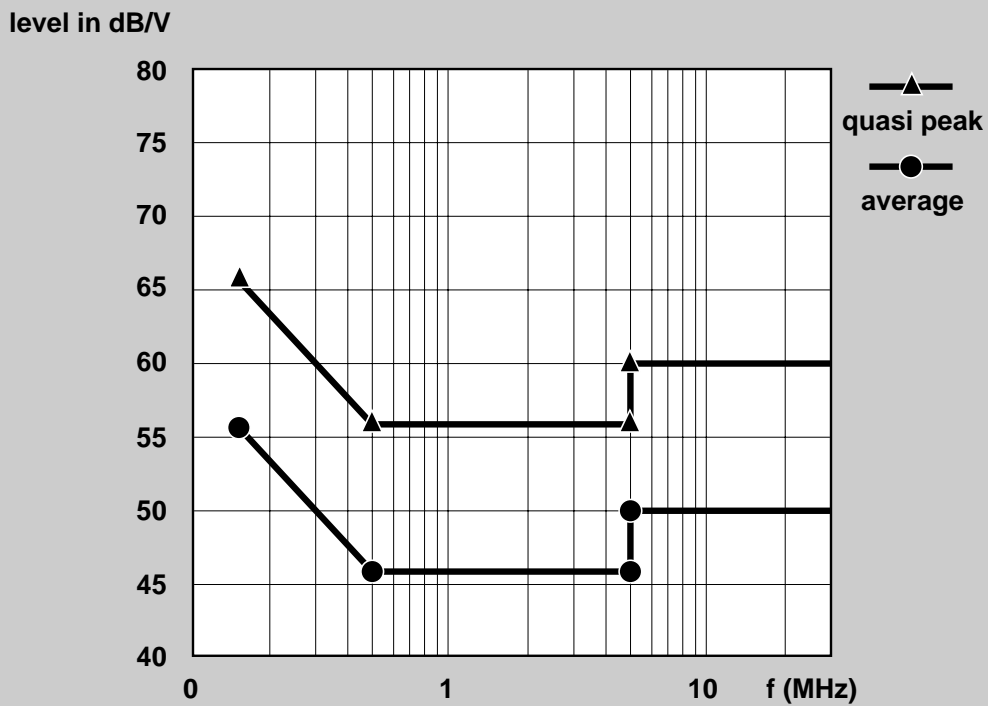


Fig.1a European generic emission norm 50081-1 (residential, commercial, light industry).

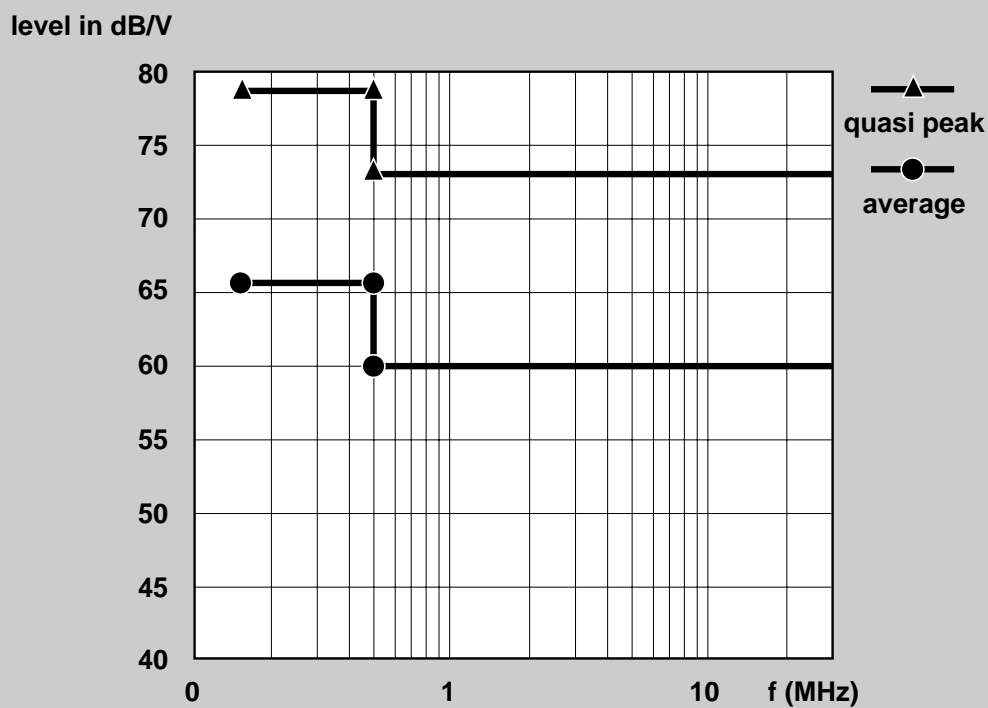


Fig.1b European generic emission norm 50081-2 (industrial environment).

At low frequency, a ferrite inductor is a low-loss, constant self-inductance. Interferences occur at elevated frequencies and there the picture changes. Losses start to increase and at a certain frequency, the ferrimagnetic resonant frequency, permeability drops rapidly and the impedance becomes almost completely resistive. At higher frequencies it even behaves like a lossy capacitor. While for most applications the operating frequency should stay well below this resonance, effective interference suppression is achieved up to much higher frequencies. The impedance peaks at the resonant frequency and the ferrite is effective in a wide frequency band around it. The material choice follows from the critical interference frequencies; ideally they should coincide with the ferrimagnetic resonance frequency, the top of the impedance curve. According to Snoek's law, this resonant frequency is inversely proportional to the initial permeability, which gives us a guide for material choice. The higher the interference frequency, the lower the material permeability should be. The whole RF spectrum can be covered with a few materials if the right permeability steps are chosen.

At the resonant frequency and above, the impedance is largely resistive, which is a favourable characteristic of ferrites.

- *Firstly*, a low-loss inductance can resonate with a capacitance in series (positive and negative reactance), leading to almost zero impedance and interference ***amplification!*** A resistor cannot resonate and is reliable independent of source and load impedances.
- *Secondly*, a resistance dissipates interfering signals rather than reflecting them to the source. Small oscillations at high frequency can damage semiconductors or negatively affect circuit operation and therefore it is better to absorb them.
- *Thirdly*, the shape of the impedance curve changes with the material losses. A lossy material will show a smooth variation of impedance with frequency and a real wideband attenuation. Interferences often have a wideband spectrum to suppress.

2.d. Current-compensation

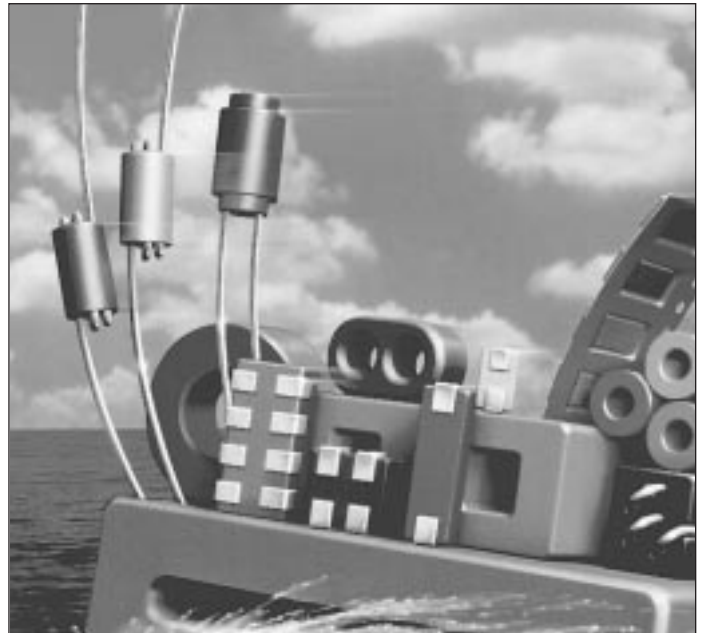
Ferrite inductors inserted separately in both lines suppress both common and differential mode interference. However, saturation by the supply current can be a problem. Remedies are a low permeability material, a gapped or open circuit core type. Disadvantage is the larger number of turns required to achieve the same inductance, leading to higher copper losses. All this can be overcome with current-compensation. Phase and null supply currents are opposite and have equal magnitude. If both conductors pass through the same holes in the ferrite core, the net current is theoretically zero and no saturation occurs. In other words, these currents generate opposite fluxes of equal magnitude that cancel out.

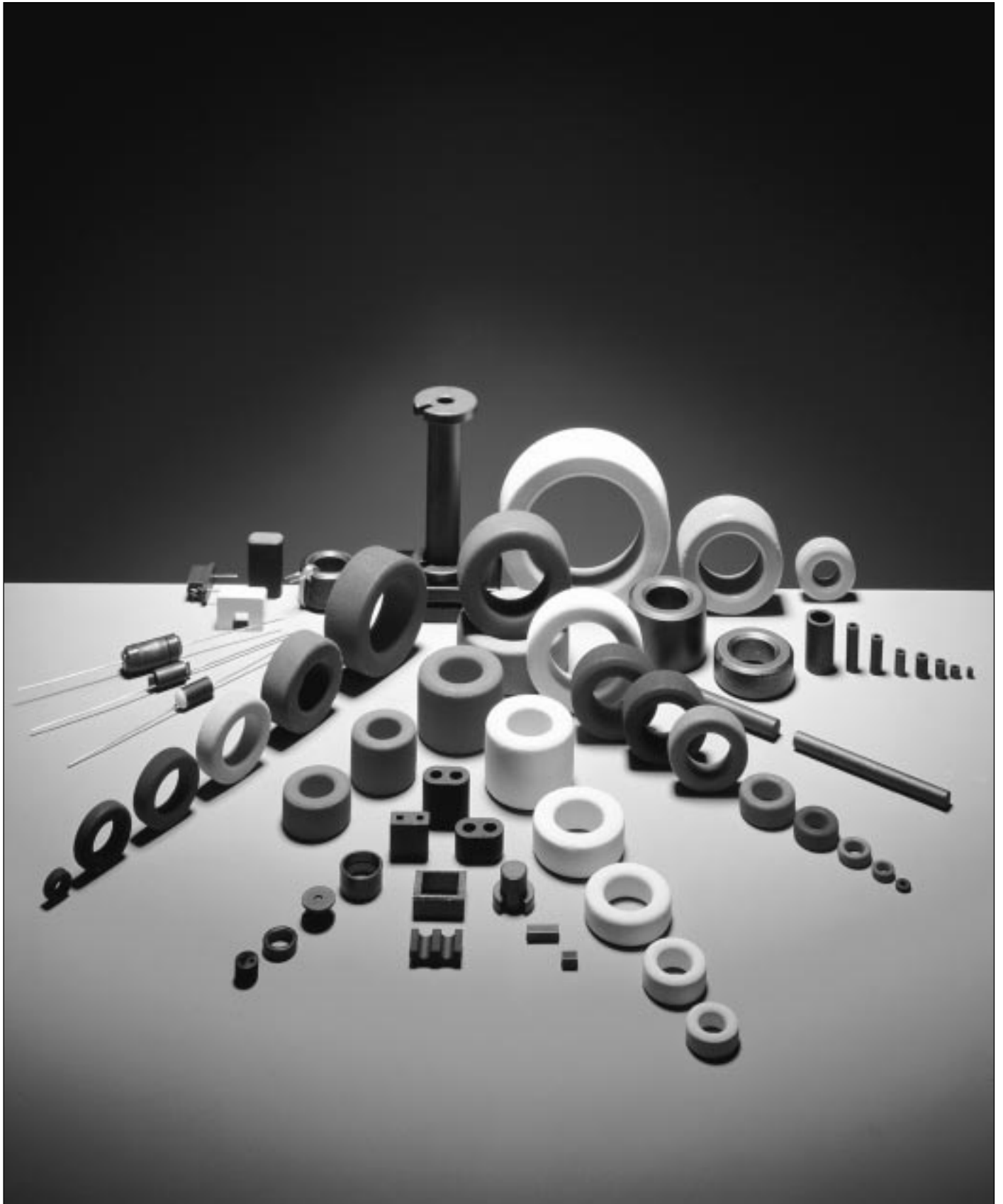
In practice, some stray flux will occur. The stray flux paths will not coincide and these fluxes do not cancel out.

Examples of current-compensated inductors:

- A ring core with two windings with equal number of turns. The winding directions are such that the incoming current through one winding and the equally large outgoing current through the other generate opposite fluxes of equal magnitude. Current-compensation would be almost ideal with both windings along the total circumference, one over the other. But in practical cases each winding is placed on one half of the ring core because of insulation requirements.
- A twisted wire inductor, which is wound with the twisted wire pair as if it were a single wire.
- A tube or round cable shield shifted on a co-axial cable.
- A flat cable shield, shifted on a flat cable. Here the net current of all inductors together is zero.

In case of an I/O cable, such as coax or flat cable, the problem will not be saturation by high current. The reason for the current-compensation is now that the actual signal is also of RF frequency and it would be suppressed together with the interference. The current-compensated inductor has one limitation: it is only active against common-mode interference. However the small leakage inductance will also suppress some differential-mode interference.





3. Material specifications

There are different material categories :

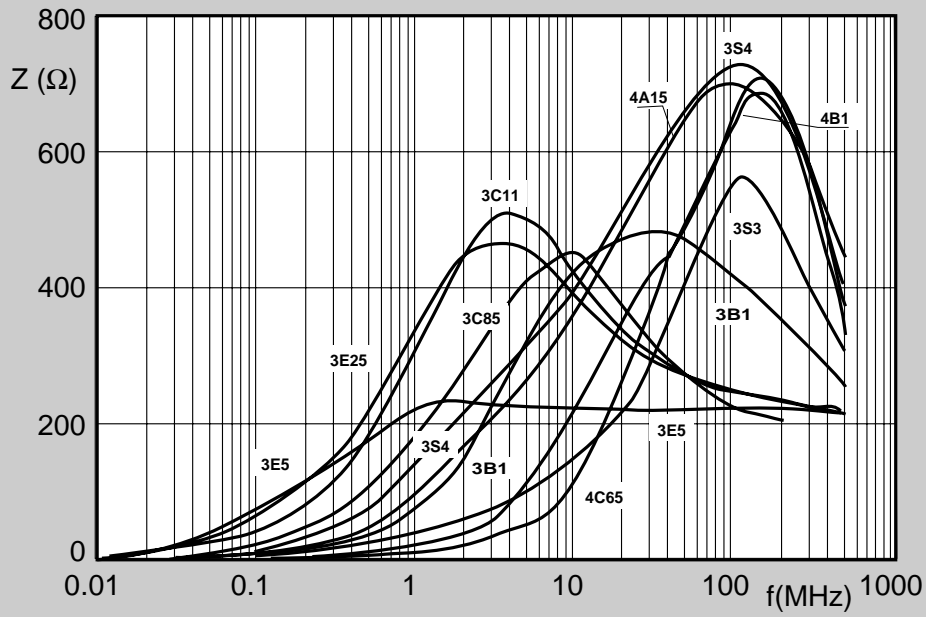
- **Manganese-zinc ferrites (MnZn)**
These ferrites have a high permeability but also a low resistivity and are most effective at low frequencies. The new ferrites 3S3 and 3S4 have a higher resistivity and are real wideband materials as well.
 - **Nickel-zinc ferrites (NiZn)**
These materials usually have a lower permeability but much higher electrical resistivity than the manganese-zinc ferrites and are effective up to 1000 MHz.
 - **Iron powder**
Permeability of this material is also low but bandwidth is less than for nickel-zinc ferrites because of their low resistivity. Their main advantage is a saturation flux density which is much higher than for ferrites, so they are suitable for very high bias currents.
- The main material parameters are given in the table while the typical impedance curves are given in Fig.3. For manganese zinc ferrites the frequency at which the

Main material parameters.

The impedance peak frequency versus permeability curve clearly confirms Snoek's law. For the nickel zinc ferrites the same law is valid, but at high frequency the picture is more complex. Apart from resonant losses, eddy current losses will play an important role. They reduce the impedance at high frequencies for manganese zinc ferrites. For nickel zinc ferrites they are not very important below 100 MHz due to the much higher resistivity. The 4A15 curve in Fig.3 peaks at 100 MHz although permeability is higher than that of 3B1. A second complicating factor is parasitic coil capacitance. The 4B1 and 4C65 curves (measured on the same ring size and with equal number of turns for comparison) are limited by coil capacitance, whereas the 4S2 curve of Fig.5 was measured on a bead (N=1) and peaks at higher frequency.

| Type | Material | μ_i | Bsat (mT) | Tc (°C) | ρ (Ωm) |
|-------------|----------|---------|-----------|---------|-----------------------------|
| Manganese | 3E7 | 15000 | 400 | 130 | 0.1 |
| Zinc | 3E6 | 12000 | 400 | 130 | 0.1 |
| | 3E5 | 10000 | 400 | 120 | 0.5 |
| | 3E25 | 6000 | 400 | 125 | 0.5 |
| | 3C11 | 4300 | 400 | 125 | 1 |
| | 3S1 | 4000 | 400 | 125 | 1 |
| | 3C85 | 2000 | 500 | 200 | 2 |
| | 3S4 | 1700 | 350 | 110 | 10^3 |
| | 3B1 | 900 | 400 | 150 | 0.2 |
| | 3S3 | 250 | 350 | 200 | 10^4 |
| Nickel | 4A15 | 1200 | 350 | 125 | 10^5 |
| Zinc | 4S2 | 700 | 350 | 125 | 10^5 |
| | 4B1 | 250 | 350 | 250 | 10^5 |
| | 4C65 | 125 | 350 | 350 | 10^5 |
| Iron powder | 2P90 | 90 | 1600 | 140* | low |





*Fig.3 Impedance versus frequency for several ferrite materials.
(measured on TN12.5/7.5/5 ring cores with 5 turns)*

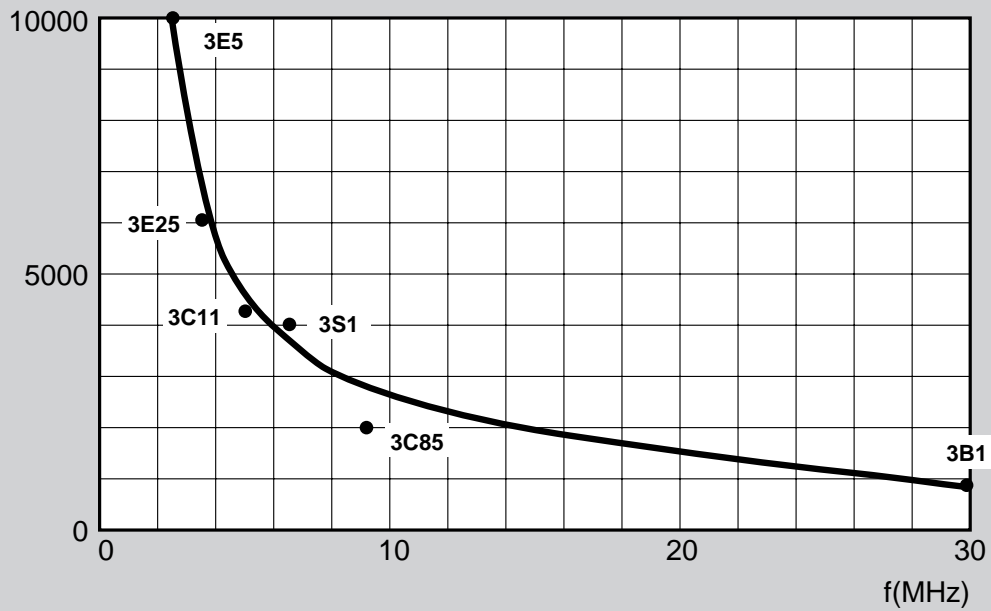


Fig.4 Frequency of impedance peak for some MnZn ferrite materials.

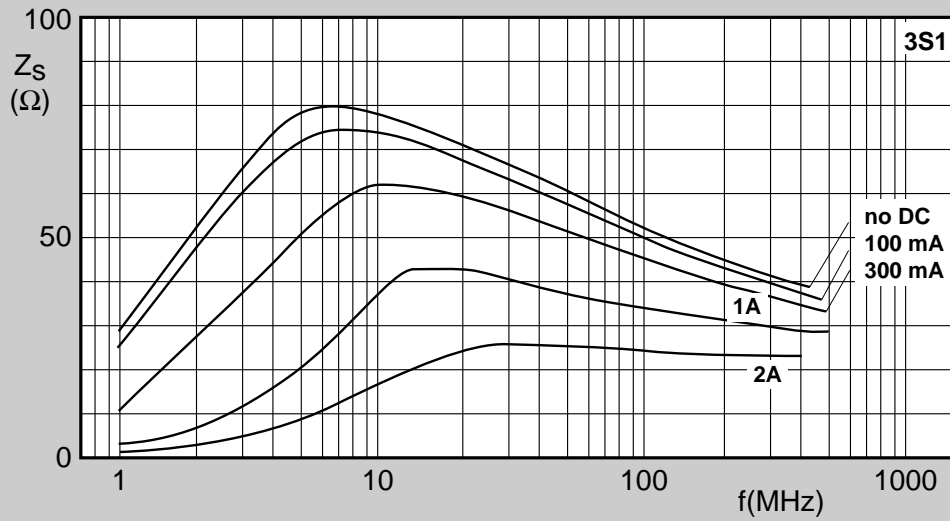


Fig.5 Effect of bias current on the impedance of a 3S1 bead.
(measured on BD5/2/10 beads on a single wire)

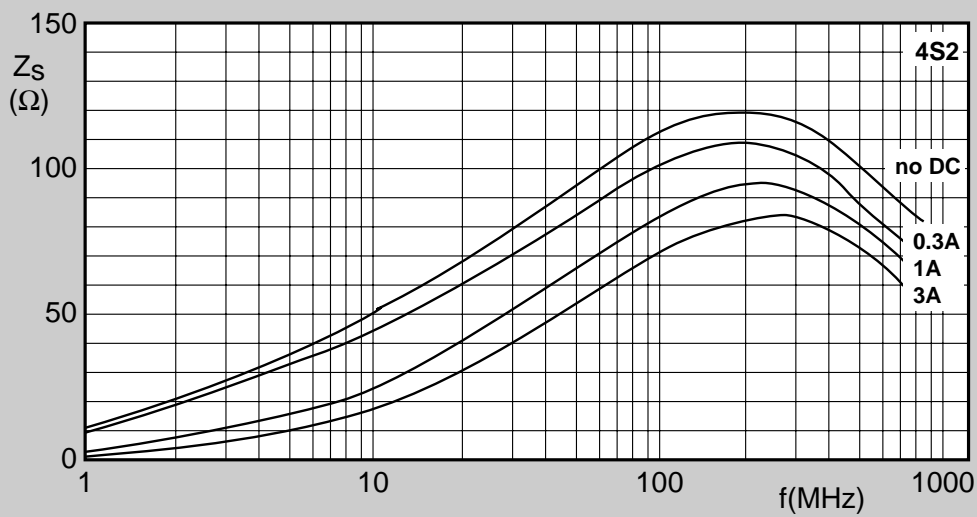


Fig.6 Effect of bias current on the impedance of a 4S2 bead.
(measured on BD5/2/10 beads on a single wire)

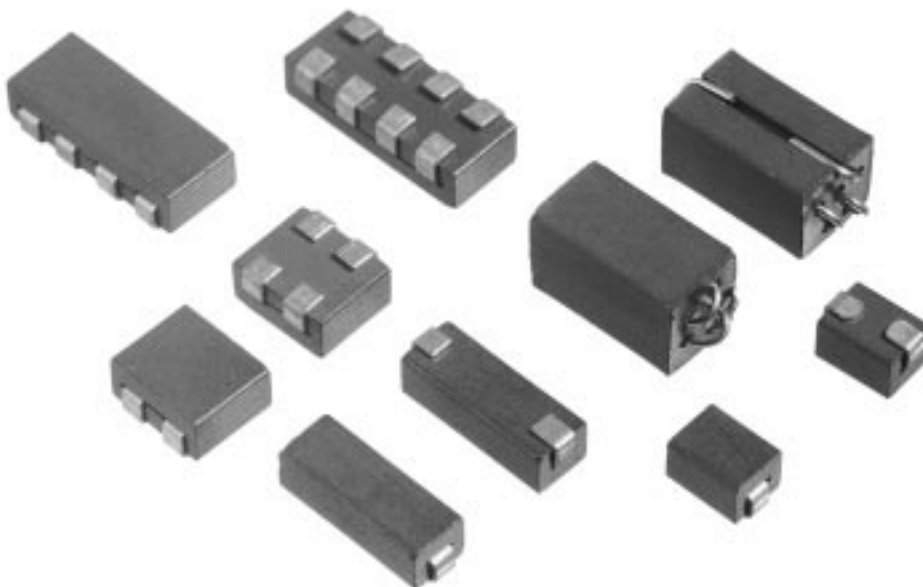
4. EMI suppression product lines

A variety of shapes is used for EMI suppression (see the table below). For most of these product types Philips Components have defined a standard range with balanced size distribution and logical material selection. Apart from the standard range, products can be custom designed to fit a specific application. Solderability and taping are in accordance with accepted IEC and EIA norms. A thorough quality control is maintained in all stages of the production process : raw materials inspection, powder

batch control, statistical process control (SPC) and production batch control as final inspection. Our production facilities are, certified to *ISO 9000*. For detailed information on product lines, ask for the appropriate product brochure, see section 7. Sample boxes are available to support the designer.

| Type | Shape | Main application |
|---------------------------|--------------------|---------------------------------|
| magnetically closed cores | ferrite ring cores | mains filters |
| | iron powder rings | lamp dimmers |
| | tubes | round cable shielding |
| | beads | wire & component lead filtering |
| | multihole cores | wire filtering (multi-turn) |
| | cable shields | round & flat cable shielding |
| | plate with holes | flat cable connector shielding |
| magnetically open cores | rods | commutation motors in cars |
| | bobbin cores | power line chokes |
| inductors | beads-on-wire | PCB supply line / RF filtering |
| | SMD beads & chokes | PCB supply line / RF filtering |
| | wideband chokes | domestic appliances, various |

Table 2: Product shapes with their main application



Range of SMD beads and chokes

5. EMI suppression applications

Whereas the material choice is derived from the EMI frequency band, the core shape and way of winding are largely determined by practical considerations and possible saturation by the load current. According to the last criterion, three application groups can be distinguished : small signal, intermediate and power.

5.a. Small signal applications

- **Coaxial cable shielding**
(round cable shield, tubes, ring cores)
- **Flat cable shielding**
(rectangular cable shield)

If the cable carries an information signal, either analog or digital, saturation will be no issue. This is typically the case with cable shielding. Inside diameter is fixed by the cable dimensions and impedance adjusted mainly by the length and / or number of shields. Impedance depends linearly on length and only logarithmically on the outside dimensions. The product can be in one piece for mounting during manufacturing or split for retrofit solution. A split product uses special clamps to prevent a parasitic air gap with loss of impedance. A very simple (temporal) retrofit solution for flexible cable is winding a few turns on a ring core of large diameter. The large inner diameter and short length (small impedance) are compensated by using more than one turn. The suppression is only common mode.

- **Cable connector shielding**
(plate with holes)

A built-in suppression for the connector of a flat cable is a ferrite plate with holes fitting over the separate pins. The material must be nickel-zinc to prevent shortcircuit. Because the holes are close together, this configuration approximates the common mode configuration of the above mentioned cable shields.



5.b. Intermediate applications

- **Component lead filtering**
(beads)

Beads are small tubes especially designed for suppression. If a specific known component is the source, e.g. a diode causing overshoot oscillations when entering the non-conductive state, then the bead is shifted directly over the leads of this component.

- **PCB inductors**
(beads-on-wire, SMD beads & chokes)

If the source is not known, but the propagation path can be identified, e.g. the DC power supply lines or a fast digital clock line, then this line should be blocked. The bead has two equivalents:

- for through-hole mounting a bead-on-wire, bead glued on a wire, axially taped and reeled.
- for surface mounting an SMD bead, bead with flat wire, blister taped and reeled.

A larger impedance can be achieved with a multi-turn choke. For even higher attenuation a complete filter can be made by adding capacitors. SMD ceramic multi-layer capacitors (CMC) are best suited for this purpose because of their very small lead inductance and excellent high-frequency characteristics.

- **Wire filtering**
(beads, two-hole cores)

If only the printed circuit board that generates the interference is known, then the wires connecting it with other system boards should be filtered. Wires can be filtered with a bead like component leads. To achieve more impedance, multihole cores are a good solution. The wire is simply drawn through several holes until sufficient impedance is achieved. The system parts are not necessarily boards. In an electric shaver for instance you will find a filter between mains plug and motor consisting often of a bead on either lead, combined with 3 capacitors.

- **Wideband chokes**

Wideband chokes are mounted on different places, often not on circuit boards. Their main advantage is a combination of high impedance and large bandwidth. The wires are wound through holes in the core, thus separating them physically and reducing parasitic coil capacitance. Several insulated types are available to prevent shortcircuit between wire bends or of wire bends with other metallic parts.

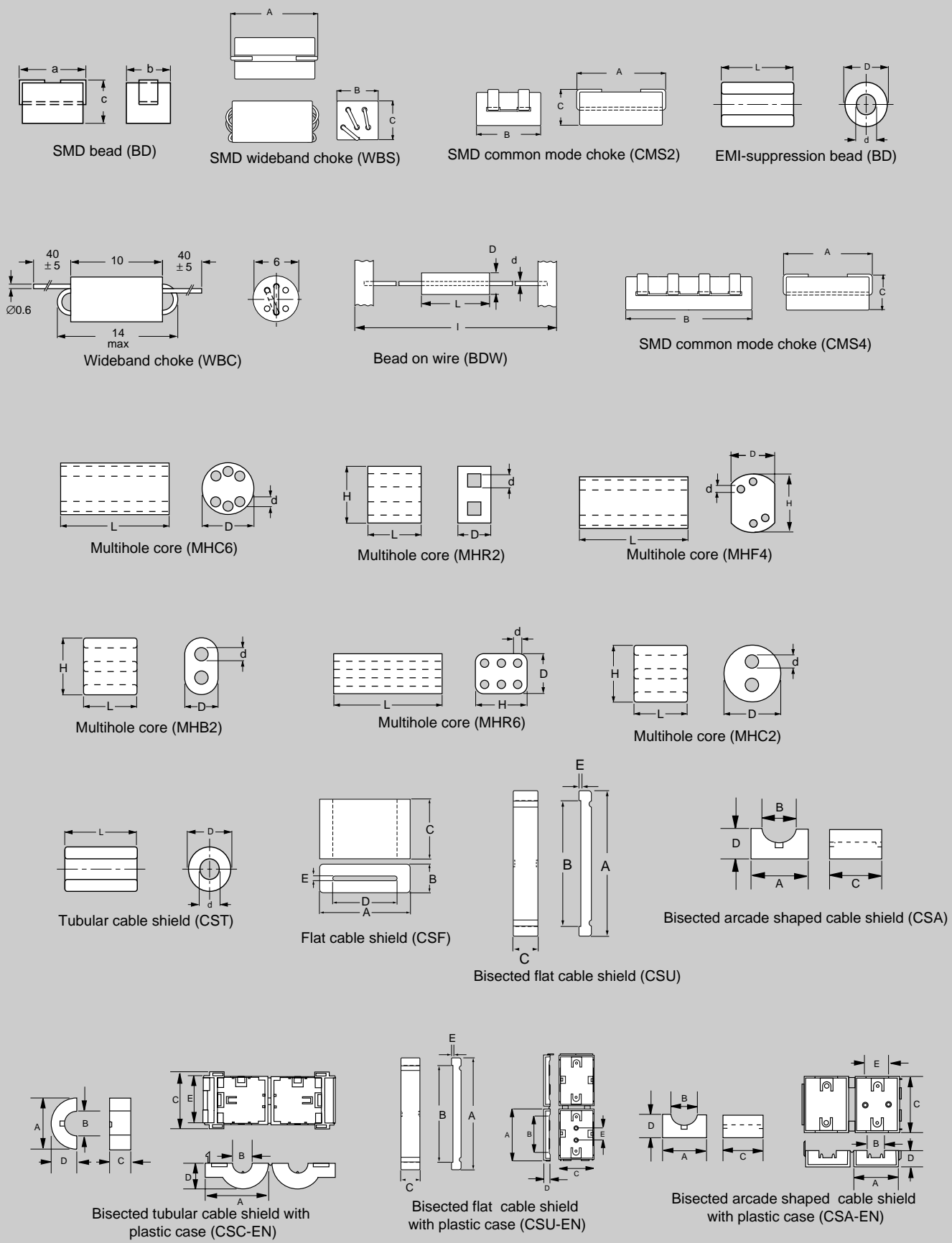


Fig 7 Overview of small signal suppression products

5.c. Power applications

- **Current-compensated chokes in mains filters**
(ferrite ring cores)

Most equipment nowadays has switched-mode power supplies to reduce volume and weight. Electronic circuits have been miniaturised constantly and the remaining subsystems set the size limits. A television set is not much more than a picture tube and a power supply. For EMC purposes, a mains filter is necessary. The same holds for the electronic ballast of energy-saving fluorescent lamps. Mains filters are also manufactured as separate components.

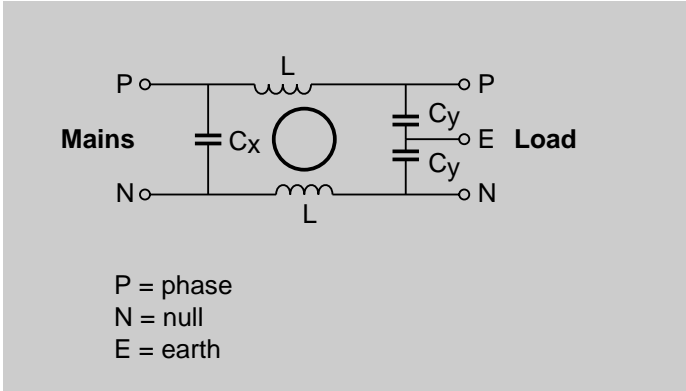


Fig 8 Typical mains filter configuration.

The following components can be found in mains filters :

- two inductors L on the same core for low-frequency attenuation (harmonics of the switching frequency)
- two C_y capacitors for additional common-mode attenuation (at higher frequencies)
- a C_x capacitor for differential-mode attenuation

The choke has to fulfil contradicting requirements : high inductance as well as high rated current. To prevent an unpractical choke size, current-compensation is applied to a ring core in a high-permeability material (see also section 2.d.). Many variations exist according to the specific equipment type, e.g. the compensated choke alone can be moulded in the plug of TV supply cables.

- **Lamp dimmers**
(iron powder ring cores)

Fluorescent lamps cannot be dimmed like incandescent lamps simply by decreasing voltage, because below their threshold they turn off. Electronic dimmers use a variable part of the supply voltage period by means of delayed thyristor ignition. The harmonics of the mains frequency require iron powder i.s.o. laminated silicon iron to reduce eddy current losses. On the ignition instant a parasitic ringing can be observed, of which the frequency (a few MHz) is determined by parasitic inductances and capacitances in the circuit. At MHz frequencies the losses of iron powder are large and the ringing is dissipated in a few periods. Ferrites have much less losses and would reflect a large part of the ringing energy, which could damage the semiconductors of the control circuitry.

- **Power line chokes**
(bobbin cores)

If chokes operate on separate power lines and current-compensation is not possible, then an open core type must be chosen. To reach a high inductance, hundreds of turns can be necessary and a bobbin core is the appropriate shape.

- **Electric commutation motors in cars**
(rods)

In a modern car, many electric commutation motors are applied. There are starter motors, a fuel pump, small ventilators, screen wiper motors, window lift motors, sun roof motors etc. The commutation is accompanied by high-frequency sparks which cause RF interference. This will be picked up by the FM radio, but if motor functions are regulated electronically, also safety is at stake. Large currents are involved, starter motor current can be as high as 30 A. Due to the frequency (FM band around 100 MHz) the inductance does not have to be very large and a rod with a single layer winding is the right choice. Motor temperatures can reach 150 °C, so the Curie temperature of the ferrite should be well over 200 °C, in combination with good HF impedance behaviour. The low permeability is no problem in a rod shape. 3S3 is the ideal material for this application.

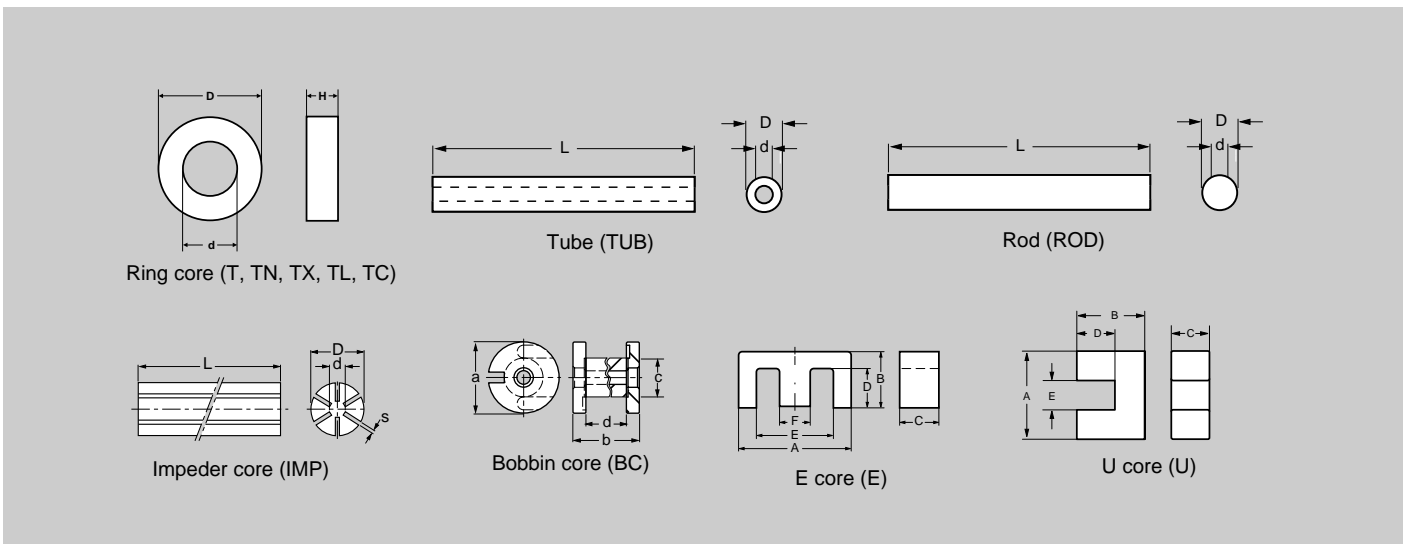


Fig 9 Some products used in power applications

6. Design considerations

Even without any trials or calculations, a lot of problems can be avoided beforehand by good design practices. In order of priority they are :

- avoid generating interference (minimize clock rate, smoothen pulse shape),
- keep it far away (separate power components and circuits from the rest)
- impede its propagation (minimize conductor path length and component lead length,
- suppress with ferrites and capacitors).

The following point should be considered while taking EMI-suppression measures:

- The insertion of ferrite components lowers equally emission and susceptibility, the essence is blocking the propagation path. The ferrite should always be located as close to the source as possible. All intermediate circuitry and cable length acts as antenna and produces radiated interference. The same holds for capacitors or any type of suppression component.
- The ferrite and the conductor should be close together. Beads, tubes and cable shields should fit close around the wire or cable and other core shapes should be wound tightly. If not, then stray flux is present, which converts into mutual inductance if other circuit part are close enough to be in the stray field.
- Especially for open core types like rods and bobbin cores, the stray flux can be a problem. Bobbin cores are better than rods. Apart from keeping distance to other circuit parts, the positioning is important. For long thin rods a horizontal position is the best. The core axis is horizontal, so the magnetic field is almost parallel to PCB and the induced electric field almost perpendicular to. This results in only low induced voltages in PCB tracks.
- For inductors with many turns, the winding method influences the parasitic coil capacitance. Too much capacitance causes early frequency roll-off of the impedance. Ways to reduce parasitic capacitance are multi-chamber winding (separation of turns in groups), and 90 degree cross-winding (electrical decoupling of adjacent turns).
- Capacitors should always be connected with leads as short as possible, because the leads have parasitic inductance (in the order of 10 nH/cm) which causes early frequency roll-off in the attenuation curve. In general filters should be layed out as compact as possible.

Appendix A. Impedance concept

A.1. Material

The impedance curve can be translated to a pure material curve, the so-called complex permeability curve. As impedance consists of a reactive and a resistive part, permeability should have two parts too to represent this. The real part corresponds to the reactance, positive for an inductance, negative for a capacitance, and the imaginary part to the losses.

$$Z = j\omega \cdot (\mu' - j\mu'') \cdot L_0 = \omega \cdot \mu'' \cdot L_0 + j\omega \cdot \mu' \cdot L_0$$

$$Z = R + jX \rightarrow R = \omega \cdot \mu'' \cdot L_0 ,$$

$$X = \omega \cdot \mu' \cdot L_0 \quad (\omega = 2 \cdot \pi \cdot f)$$

$$Z = \sqrt{(R^2 + X^2)} = \omega \cdot L_0 \cdot \sqrt{(\mu'^2 + \mu''^2)}$$

Where L_0 is the inductance if initial permeability were equal to 1 :

$$L_0 = \mu_0 \cdot n^2 \cdot A_e / l_e$$

$$(\mu_0 = 4 \pi \times 10^{-7} = 1.2566 \times 10^{-6} \text{ [H/m)})$$

For the calculation of effective magnetic dimensions A_e and l_e , see next paragraph.

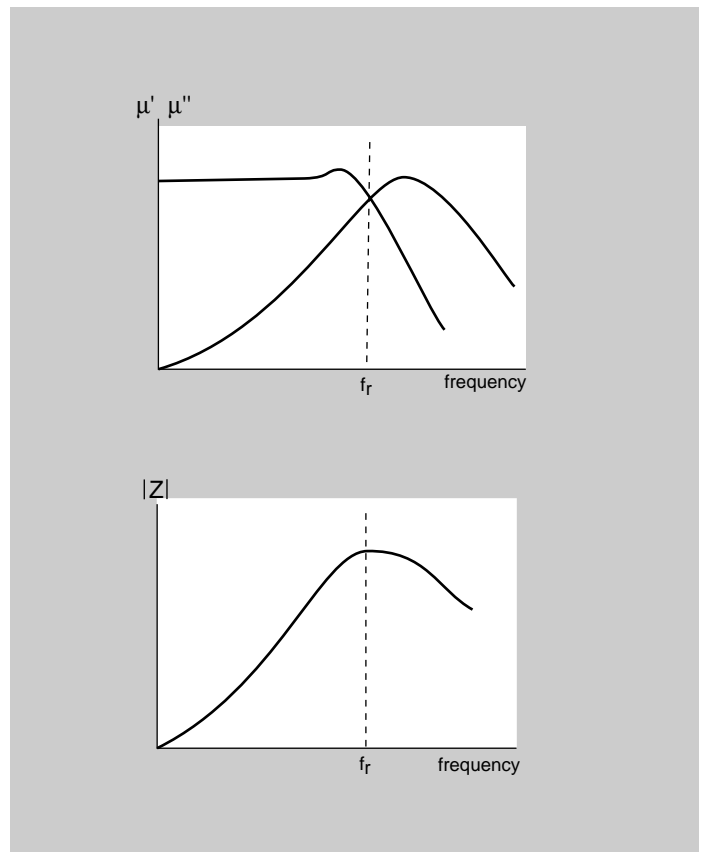


Fig.10 Complex permeability and impedance.

A.2. Core size

The choice of a suppression product is made in two steps. First the material choice corresponding to the interference frequencies occurring and afterwards the right core size and turns for the impedance level required.

The simplest way of calculation is taking the impedance curve of a reference core of the same material. Calculation from complex permeability is another possibility, but it's more bothersome. Two factors have to be corrected : effective magnetic dimensions and turns.

$$Z :: N^2 \cdot A_e / l_e \rightarrow$$

$$Z = Z_0 \cdot (N^2 / N_0^2) \cdot (A_e / A_{e0}) \cdot (l_{e0} / l_e)$$

where the parameters with index **o** correspond to the reference core. The number of turns **N** is always an integer number. Half a turn geometrically is 1 turn magnetically. For a bead with a single wire going through, **N = 1** turn. The effective magnetic dimensions **A_e** (area) and **l_e** (length) are calculated from geometric dimensions according to IEC 205. For complicated geometries this involves complex formulas. Therefore the suppliers usually specify these data in their handbooks. For a cylindrical geometry (ring core, tube, bead, bead-on-wire) a simple formula applies:

$$A_e / l_e = h / (2 \cdot \pi) \cdot \ln(OD/ID)$$

OD = outer diameter

ID = inner diameter

h = height

A.3. Bias current

Often a DC supply or AC mains current is passing through the inductor to allow normal operation of the connected equipment. This current induces a high field strength in the ferrite core, which can lead to saturation. Impedance then decreases along with permeability, especially for low frequencies. The influence of a bias current can be calculated. The induced field strength is directly proportional to the current :

$$H = n \cdot I / l_e$$

Whether this field causes a significant saturation or not, can be seen in the curve of permeability versus bias field. However, this only indicates the decrease of inductance at low frequency. The impedance at high frequency decreases less. Again, impedance can be calculated from reference curves if they show impedance versus frequency with bias current as a parameter.

First, bias current is translated to the current that would induce the same field strength in the reference core, which means the same state of core saturation :

$$I_0 = I \cdot (n/n_0) \cdot (l_{e0}/l_e)$$

For a ring core, tube or bead the effective length is

$$l_e = \pi \cdot \ln(OD/ID) / (1/ID - 1/OD)$$

Now the relative impedance decrease will be the same :

$$Z_{\text{bias}} = Z \cdot (Z_0 \text{ bias} / Z_0)$$

Literature and Sample Boxes

| Ordering code | title |
|---------------------------|--|
| General catalogues | |
| 9398 184 01011 | Handbook MA01: Soft ferrites |
| 9398 237 02011 | Product Selection Guide |
| Specific brochures | |
| 9398 235 68011 | SMD Beads and Chokes |
| 9398 387 00011 | Wideband Chokes |
| 9398 236 27011 | Cable Shielding |
| 9398 082 81011 | Power Inductors |
| 9398 083 34011 | 3S4 a new Soft Ferrite for EMI-suppression |
| 9398 083 37011 | 3S3 a new Soft Ferrite for EMI-suppression |
| Sample boxes | |
| SAMPLEBOX9 | SMD Beads and Chokes |
| SAMPLEBOX10 | Cable Shielding |
| SAMPLEBOX11 | EMI-suppression Products |

Magnetic Products NAFTA Sales Offices

| | | |
|--------------------------------|---|----------------|
| Alabama | Over and Over, Inc., Charlotte, NC | (708) 583-9100 |
| Alaska | Eclipse Marketing Group, Redmond, WA | (206) 885-6991 |
| Arizona | Harper and Two, Tempe, AZ | (602) 804-1290 |
| Arkansas | Philips Components, Willoughby, OH | (440) 269-8585 |
| California - Northern | Criterion Sales, Santa Clara, CA | (408) 988-6300 |
| California - Southern | Harper and Two, Signal Hill, CA | (801) 264-8050 |
| Colorado | Philips Components, Willoughby, OH | (440) 269-8585 |
| Connecticut | Philips Components, Woburn, MA | (617) 932-4748 |
| Delaware | Philips Components, Woburn, MA | (617) 932-4748 |
| Florida | Over and Over, Charlotte, NC | (704) 583-9100 |
| Georgia | Over and Over, Charlotte, NC | (704) 583-9100 |
| Hawaii | Harper and Two, Signal Hill, CA | (310) 424-3030 |
| Idaho - Northern | Eclipse Marketing Group, Redmond, WA | (206) 885-6991 |
| Idaho - Southern | Electrodyne, Inc., Salt Lake City, UT | (801) 264-8050 |
| Illinois - Northern | Philips Components, Willoughby, OH | (440) 269-8585 |
| Illinois - Quad Cities | Lorenz Sales, Cedar Rapids, IA | (319) 377-4666 |
| Illinois - Southern | Lorenz Sales, St. Louis, MO | (314) 997-4558 |
| Indiana - Northern | Corrao Marsh, Fort Wayne, IN | (219) 482-2725 |
| Indiana - Central and Southern | Corrao Marsh, Greenfield, IN | (317) 462-4446 |
| Iowa - All except Quad Cities | Lorenz Sales, Cedar Rapids, IA | (319) 377-4666 |
| Kansas - Northeast | Lorenz Sales, Overland Park, KS | (913) 469-1312 |
| Kansas - All except Northeast | Lorenz Sales, Wichita, KS | (316) 721-0500 |
| Kentucky | Corrao Marsh, Greenfield, IN | (317) 462-4446 |
| Louisiana | Philips Components, Willoughby, OH | (440) 269-8585 |
| Maine | Philips Components, Woburn, MA | (617) 932-4748 |
| Maryland | Philips Components, Willoughby, OH | (440) 269-8585 |
| Massachusetts | Philips Components, Woburn, MA | (617) 932-4748 |
| Michigan | Philips Components, Willoughby, OH | (440) 269-8585 |
| Minnesota | Electronic Component Sales, Minneapolis, MN | (612) 946-9510 |
| Mississippi | Over and Over, Charlotte, NC | (704) 583-9100 |
| Missouri - Eastern | Lorenz Sales, St. Louis, MO | (314) 997-4558 |
| Missouri - Western | Lorenz Sales, Overland Park, KS | (913) 469-1312 |
| Montana | Electrodyne, Inc., Salt Lake City, UT | (801) 264-8050 |
| Nebraska | Lorenz Sales, Cedar Rapids, IA | (319) 377-4666 |
| Nevada - Central and Northern | Criterion Sales, Santa Clara, CA | (408) 988-6300 |
| Nevada - Southern | Harper and Two, Tempe, AZ | (602) 804-1290 |
| New Hampshire | Philips Components, Woburn, MA | (617) 932-4748 |
| New Jersey | Philips Components, Woburn, MA | (617) 932-4748 |
| New Mexico | Harper and Two, Tempe, AZ | (602) 804-1290 |
| New York - Western | Philips Components, Willoughby, OH | (440) 269-8585 |
| New York - All other | Philips Components, Woburn, MA | (617) 932-4748 |
| North Carolina | Over and Over, Charlotte, NC | (704) 583-9100 |
| North Dakota | Electronic Component Sales, Minneapolis, MN | (612) 946-9510 |
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| Oklahoma | Philips Components, Willoughby, OH | (440) 269-8585 |
| Oregon | Eclipse Marketing Group, Beaverton, OR | (503) 642-1661 |
| Pennsylvania - Western | Philips Components, Willoughby, OH | (440) 269-8585 |
| Pennsylvania - Eastern | Philips Components, Woburn, MA | (617) 932-4748 |
| Rhode Island | Philips Components, Woburn, MA | (617) 932-4748 |
| South Carolina | Over and Over, Charlotte, NC | (704) 583-9100 |
| South Dakota | Electronic Component Sales, Minneapolis, MN | (612) 946-9510 |
| Tennessee | Over and Over, Charlotte, NC | (704) 583-9100 |
| Texas | Philips Components, Willoughby, OH | (440) 269-8585 |
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| Mexico | Philips Components, El Paso, TX | (915) 772-4020 |
| Puerto Rico | Max Anderson Co., Caperra Heights, PR | (809) 783-6544 |
| Virgin Islands | Max Anderson Co., Caperra Heights, PR | (809) 783-6544 |

Philips Components – a worldwide company

Australia: Philips Components Pty Ltd., NORTH RYDE,
Tel. +61 2 9805 4455, Fax. +61 2 9805 4466

Austria: Österreichische Philips Industrie GmbH, WIEN,
Tel. +43 1 60 101 12 41, Fax. +43 1 60 101 12 11

Belarus: Philips Office Belarus, MINSK,
Tel. +375 172 200 924/733, Fax. +375 172 200 773

Benelux: Philips Nederland B.V., EINDHOVEN, NL,
Tel. +31 40 2783 749, Fax. +31 40 2788 399

Brazil: Philips Components, SÃO PAULO,
Tel. +55 11 821 2333, Fax. +55 11 829 1849

Canada: Philips Electronics Ltd., SCARBOROUGH,
Tel. +1 416 292 5161, Fax. +1 416 754 6248

China: Philips Company, SHANGHAI,
Tel. +86 21 6354 1088, Fax. +86 21 6354 1060

Denmark: Philips Components A/S, COPENHAGEN S,
Tel. +45 32 883 333, Fax. +45 31 571 949

Finland: Philips Components, ESPOO,
Tel. +358 9 615 800, Fax. +358 9 615 80510

France: Philips Composants, SURESNES,
Tel. +33 1 4099 6161, Fax. +33 1 4099 6493

Germany: Philips Components GmbH, HAMBURG,
Tel. +49 40 2489-0, Fax. +49 40 2489 1400

Greece: Philips Hellas S.A., TAVROS,
Tel. +30 1 4894 339/+30 1 4894 239, Fax. +30 1 4814 240

Hong Kong: Philips Hong Kong, KOWLOON,
Tel. +852 2784 3000, Fax. +852 2784 3003

India: Philips India Ltd., MUMBAI,
Tel. +91 22 4930 311, Fax. +91 22 4930 966/4950 304

Indonesia: P.T. Philips Development Corp., JAKARTA,
Tel. +62 21 794 0040, Fax. +62 21 794 0080

Ireland: Philips Electronics (Ireland) Ltd., DUBLIN,
Tel. +353 1 7640 203, Fax. +353 1 7640 210

Israel: Rapac Electronics Ltd., TEL AVIV,
Tel. +972 3 6450 444, Fax. +972 3 6491 007

Italy: Philips Components S.r.l., MILANO,
Tel. +39 2 6752 2531, Fax. +39 2 6752 2557

Japan: Philips Japan Ltd., TOKYO,
Tel. +81 3 3740 5135, Fax. +81 3 3740 5035

Korea (Republic of): Philips Electronics (Korea) Ltd., SEOUL,
Tel. +82 2 709 1472, Fax. +82 2 709 1480

Malaysia: Philips Malaysia SDN Berhad,
Components Division, PULAU PINANG,
Tel. +60 3 750 5213, Fax. +60 3 757 4880

Mexico: Philips Components, EL PASO, U.S.A.,
Tel. +52 915 772 4020, Fax. +52 915 772 4332

New Zealand: Philips New Zealand Ltd., AUCKLAND,
Tel. +64 9 815 4000, Fax. +64 9 849 7811

Norway: Norsk A/S Philips, OSLO,
Tel. +47 22 74 8000, Fax. +47 22 74 8341

Pakistan: Philips Electrical Industries of Pakistan Ltd., KARACHI,
Tel. +92 21 587 4641-49, Fax. +92 21 577 035/+92 21 587 4546

Philippines: Philips Semiconductors Philippines Inc.,
METRO MANILA, Tel. +63 2 816 6345, Fax. +63 2 817 3474

Poland: Philips Poland Sp. z.o.o., WARSZAWA,
Tel. +48 22 612 2594, Fax. +48 22 612 2327

Portugal: Philips Portuguesa S.A.,
Philips Components: LINDA-A-VELHA,
Tel. +351 1 416 3160/416 3333, Fax. +351 1 416 3174/416 3366

Russia: Philips Russia, MOSCOW,
Tel. +7 95 755 6918, Fax. +7 95 755 6919

Singapore: Philips Singapore Pte Ltd., SINGAPORE,
Tel. +65 350 2000, Fax. +65 355 1758

South Africa: S.A. Philips Pty Ltd., JOHANNESBURG,
Tel. +27 11 470 5911, Fax. +27 11 470 5494

Spain: Philips Components, BARCELONA,
Tel. +34 93 301 63 12, Fax. +34 93 301 42 43

Sweden: Philips Components AB, STOCKHOLM,
Tel. +46 8 5985 2000, Fax. +46 8 5985 2745

Switzerland: Philips Components AG, ZÜRICH,
Tel. +41 1 488 22 11, Fax. +41 1 481 7730

Taiwan: Philips Taiwan Ltd., TAIPEI,
Tel. +886 2 2134 2900, Fax. +886 2 2134 2929

Thailand: Philips Electronics (Thailand) Ltd., BANGKOK,
Tel. +66 2 745 4090, Fax. +66 2 398 0793

Turkey: Türk Philips Ticaret A.S., GÜLTEPE/ISTANBUL,
Tel. +90 212 279 2770, Fax. +90 212 282 6707

United Kingdom: Philips Components Ltd., DORKING,
Tel. +44 1306 512 000, Fax. +44 1306 512 345

United States:

- Display Components, ANN ARBOR, MI,
Tel. +1 734 996 9400, Fax. +1 734 761 2776
- Magnetic Products, SAUGERTIES, NY,
Tel. +1 914 246 2811, Fax. +1 914 246 0487
- Passive Components, SAN JOSE, CA,
Tel. +1 408 570 5600, Fax. +1 408 570 5700

Yugoslavia (Federal Republic of): Philips Components, BELGRADE,
Tel. +381 11 625 344/373, Fax. +381 11 635 777

Internet:

- Display Components: www.dc.comp.philips.com
- Passive Components: www.passives.comp.philips.com

For all other countries apply to:

Philips Components, Building BF-1, P.O. Box 218, 5600 MD EINDHOVEN,
The Netherlands, Fax. +31-40-27 23 903.

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